

## A Study on Misaligned Modulated Apertures in Confocal Scanning Laser Microscope (CSLM)

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### ABSTRACT

In this paper, we consider misaligned linear and quadratic apertures in the optical system of the CSLM. Tilting and lateral shift of the 2nd aperture is considered while the 1st objective is assumed aligned. The Point Spread Function (PSF), in both cases of linear and quadratic misaligned apertures, is computed the Result Point Spread Function (RPSF) for the CSLM is computed from the product of the PSF corresponding to each objective lens. A comparison of the PSF in case of misaligned apertures with that of aligned apertures is given. The input bone marrow image, using the misaligned apertures, is processed considering the CSLM. The output images are computed from the modulus square of the convolution product of the input image and the RPSF computed for the aligned and the misaligned apertures. An empirical formula for the Coherent Transfer Function (CTF) corresponding to the misaligned linear and quadratic apertures is obtained. A comparison of the CTF in both cases of aligned and misaligned objectives is given. In addition, the contrast of the reconstructed images is computed in both cases of aligned and misaligned apertures and compared with the contrast of the original image.

**Keywords:** Misaligned Linear And Quadratic Apertures, Image Processing, The Resultant Point Spread Function In CSLM.

### INTRODUCTION

The famous work on the PSF is made by Sheppard et. al. [1-12] using annular and Gaussian apertures. Improvement of axial resolution in confocal microscopy using annular pupil is investigated in [9]. Practical limits of resolution in confocal and nonlinear microscopy is presented in [11]. The effect of numerical aperture on interference fringe spacing is shown in [13]. Linear, quadratic, B/W concentric annuli, and graded index apertures is suggested by Hamed et. al. [14-20]. They computed the PSF considering the above modulated apertures giving lateral resolution improvement. Image analysis of modified Hamming aperture and an application on confocal microscopy and holography is given in [20]. Modulated-alignment dual-axis (MAD) confocal microscopy for deep optical sectioning in tissues is presented in [21]. While an image scanning microscopy with a quadrant detector is recently investigated [22].

Since few studies on the aberration and displacement of objective lenses due to misaligned optics are presented [17], hence this

study on the misaligned linear and quadratic apertures applied on the CSLM is made.

It is easy to align the first objective lens of the CSLM, while it is not the case for the second objective. Hence, we assume that the later objective is subjected to tilting and to a lateral shift with respect to the first aligned objective. The PSF in case of misaligned linear and quadratic apertures is computed and compared with the precedent study made by Hamed in [17, 18], in case of misaligned transparent circular apertures. In addition, the CTF in case of aligned and misaligned objectives provided with linear and quadratic apertures is computed. Finally, the contrast of the reconstructed images using the CSLM in different combinations of aligned and misaligned apertures using linear and quadratic apertures is discussed.

### THEORETICAL ANALYSIS

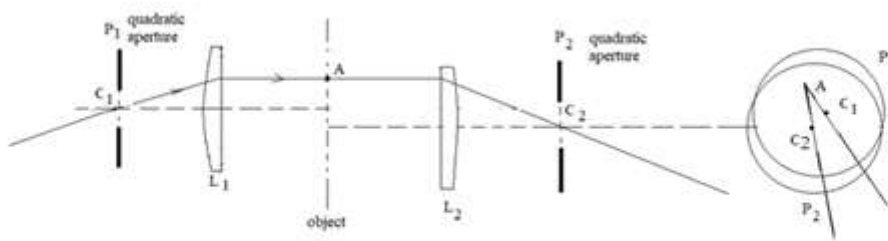
In this study, we investigate the PSF in case of misaligned linear and quadratic apertures.

Consider the CSLM under investigation as shown in the figure (1), where the first objective is aligned perfectly and the second objective is

displaced laterally by a radial amount of  $\rho_d$ . In this case, we write the complex amplitude as the first aligned aperture of linear distribution as follows:

$$P_1(\rho; \alpha) = \rho \exp[jk \rho \sin(\alpha)] ; \quad \left| \frac{\rho}{\rho_{01}} \right| \leq 1 \quad (1)$$

Where  $j = \sqrt{-1}$ ,  $k = 2\pi/\lambda$ ,  $\rho$  is the radial coordinate in the aperture plane



**Figur1.** Set- up of misaligned optical system with laterally displaced objectives using quadratic apertures in the CSLM.

While the complex amplitude for the second displaced linear aperture is written as follows:

$$P_2(\rho; \beta, \rho_d) = (\rho - \rho_d) \exp[jk \rho \sin(\beta)] ; \quad \left| \frac{\rho}{\rho_{02}} \right| \leq 1 \quad (2)$$

Where  $\alpha$ ,  $\beta$  are the tilting angles of the corresponding objectives  $L_1$  and  $L_2$ .

Similar equations are written, for the quadratic apertures where the first objective is aligned while the second is laterally displaced, as follows:

$$P_3(\rho; \alpha) = \rho^2 \exp[jk \rho \sin(\alpha)] ; \quad \left| \frac{\rho}{\rho_{01}} \right| \leq 1 \quad (3)$$

$$P_4(\rho; \beta, \rho_d) = (\rho - \rho_d)^2 \exp[jk \rho \sin(\beta)] ; \quad \left| \frac{\rho}{\rho_{02}} \right| \leq 1 \quad (4)$$

Making use of the Fourier transform operations and convolution product, we are able to get the PSF corresponding to each aperture as follows:

The PSF for the first aligned linear aperture, represented by equation (1), is solved to give the following result:

$$\begin{aligned} h_1(r) &= F.T. [P_1(\rho; \alpha)] = F.T. \{ \rho \exp[jk \rho \sin(\alpha)] \} \\ &= F.T. \{ \rho \} \otimes F.T. \{ \exp[jk \rho \sin(\alpha)] \} \\ &= F.T. \{ \rho \} \otimes \delta(r - f \sin \alpha) \end{aligned} \quad (5)$$

$$\text{Since } F.T. \{ \rho \} = 2\pi \left[ \frac{J_1(W)}{W} + \frac{J_0(W)}{W^2} - 2 \sum_i \frac{J_i(W)}{W^3} \right]; \text{ ref. [15]} \quad (6)$$

From equations 5 and 6, we finally get  $h_1$  for the 1<sup>st</sup> aligned linear aperture as follows:

$$h_1(W; \alpha) = 2\pi \left[ \frac{J_1(W')}{W'} + \frac{J_0(W')}{W'^2} - 2 \sum_i \frac{J_i(W')}{W'^3} \right] \quad (7)$$

where  $w' = \frac{2\pi\rho_{01}}{\lambda f} (r - f \sin \alpha)$  is the reduced coordinate in the Fourier plane.

The PSF for the displaced linear aperture represented by equation (2) is solved by operating the F.T. to give the following result:

$$h_2(r) = F.T. \{ (\rho - \rho_d) \exp[jk \rho \sin(\beta)] \}$$

$$\begin{aligned}
 &= F.T. \{(\rho) \exp[jk \rho \sin(\beta)]\} - F.T. \{(\rho_d) \exp[jk \rho \sin(\beta)]\} \\
 &= F.T. [(\rho)] \otimes F.T. \{ \exp[jk \rho \sin(\beta)]\} - (\rho_d) F.T. \{ \exp[jk \rho \sin(\beta)]\} \\
 &= [ F.T. (\rho) ] \otimes \delta(r - f \sin \beta) - (\rho_d) \delta(r - f \sin \beta) \\
 &= \left\{ 2\pi \left[ \frac{J_1(W)}{W} + \frac{J_0(W)}{W^2} - 2 \sum_i \frac{J_i(W)}{W^3} \right] \right\} \otimes \delta(r - f \sin \beta) - (\rho_d) \delta(r - f \sin \beta) \tag{8}
 \end{aligned}$$

We finally, get the following result for the PSF:

$$h_2(W; \beta, \rho_d) = 2\pi \left[ \frac{J_1(W'')}{W''} + \frac{J_0(W'')}{W''^2} - 2 \sum_i \frac{J_i(W'')}{W''^3} \right] - (\rho_d) \delta(r - f \sin \beta) \tag{9}$$

Where  $W'' = \frac{2\pi\rho_{02}}{\lambda f} (r - f \sin \beta)$  is the reduced coordinate in the Fourier plane.

Hence, the resultant PSF for the CSLM provided with linear apertures one aligned while the second misaligned is computed from the following equation:

$$h_r(\text{linear apert.}) = h_1(W; \alpha) \cdot h_2(W; \beta, \rho_d) \tag{10}$$

In case of quadratic aperture, the PSF for the first aligned quadratic aperture, represented by equation (3), is solved to give the following result:

$$\begin{aligned}
 h_3(r) &= F.T. \{ \rho^2 \exp[jk \rho \sin(\alpha)] \} ; \\
 &= F.T. \{ \rho^2 \} \otimes F.T. \{ \exp[jk \rho \sin(\alpha)] \} \\
 &= F.T. \{ \rho^2 \} \otimes \delta(r - f \sin \alpha) \tag{11}
 \end{aligned}$$

$$\text{Since } F.T. \{ \rho^2 \} = 2\pi \left[ \frac{J_1(W)}{W} - 2 \frac{J_2(W)}{W^2} \right]; \text{ ref. [16]} \tag{12}$$

From equations 11 and 12, we finally get  $h_3$  for the 1<sup>st</sup> aligned quadratic aperture as follows:

$$h_3(W; \alpha) = 2\pi \left[ \frac{J_1(W')}{W'} - 2 \frac{J_2(W')}{W'^2} \right] \tag{13}$$

Where  $W'$  is defined as for the linear aperture.

While the PSF for the displaced quadratic aperture represented by equation (4) is solved by operating the F.T. to give the following result:

$$\begin{aligned}
 h_4(r) &= F.T. \{ (\rho - \rho_d)^2 \exp[jk \rho \sin(\beta)] \} \tag{14} \\
 &= F.T. \{ (\rho^2 - 2\rho\rho_d + \rho_d^2) \exp[jk \rho \sin(\beta)] \} \\
 &= F.T. \{ \rho^2 \exp[jk \rho \sin(\beta)] \} - 2\rho_d F.T. \{ \rho \exp[jk \rho \sin(\beta)] \} + \rho_d^2 F.T. \{ \exp[jk \rho \sin(\beta)] \}
 \end{aligned}$$

The 1<sup>st</sup> term is given for the aligned quadratic aperture represented in equation (12), the 2<sup>nd</sup> term is given in equation (7) multiplied by a constant value  $2\rho_d$ , while the 3<sup>rd</sup> term is simply shifted Dirac-delta function located at  $f \sin \beta$  in the Fourier plane of radial coordinate  $r$  and multiplied by the shift squared  $\rho_d^2$ .

Finally, the PSF for the 2<sup>nd</sup> shifted quadratic aperture is obtained as follows:

$$\begin{aligned}
 h_4(W; \beta, \rho_d) &= 2\pi \left\{ \left[ \frac{J_1(W'')}{W''} - 2 \frac{J_2(W'')}{W''^2} \right] - 2\rho_d \left[ \frac{J_1(W'')}{W''} + \frac{J_0(W'')}{W''^2} - 2 \sum_i \frac{J_i(W'')}{W''^3} \right] \right\} \\
 &+ \rho_d^2 \delta(r - f \sin \beta) \tag{15}
 \end{aligned}$$

Where  $W''$  is defined as in the case of shifted linear aperture.

The RPSF for the CSLM provided with quadratic apertures one aligned while the second misaligned is computed from the following equation:

$$h_r(\text{quadratic apert.}) = h_3(W; \alpha) \cdot h_4(W; \beta, \rho_d) \tag{16}$$

For collimated parallel rays incident upon the apertures, the inclination angles  $\alpha, \beta$  are equal to zero. Hence, the PSF represented by equations 7, 9, 13, and 15 becomes:

$$h_1(W) = 2\pi \left[ \frac{J_1(W)}{W} + \frac{J_0(W)}{W^2} - 2 \sum_i \frac{J_i(W)}{W^3} \right]; \text{ 1st aligned linear aperture} \tag{17}$$

$$h_2(W; \rho_d) = 2\pi \left[ \frac{J_1(W)}{W} + \frac{J_0(W)}{W^2} - 2 \sum_i \frac{J_i(W)}{W^3} \right] - (\rho_d) \delta(r); \text{ 2nd shifted linear aperture} \tag{18}$$

$$h_3(W) = 2\pi \left[ \frac{J_1(W)}{W} - 2 \frac{J_2(W)}{W^2} \right]; \text{ 1st aligned quadratic aperture} \tag{19}$$

$$h_4(W; \rho_d) = 2\pi \left\{ \left[ \frac{J_1(W)}{W} - 2 \frac{J_2(W)}{W^2} \right] - 2\rho_d \left[ \frac{J_1(W)}{W} + \frac{J_0(W)}{W^2} - 2 \sum_i \frac{J_i(W)}{W^3} \right] \right\} + \rho_d^2 \delta(r); \text{ 2nd shifted quadratic aperture} \tag{20}$$

From equations 17, 18 we get the following result for the effective PSF as:

$$\begin{aligned} h_{eff}(\text{linear apert.}) &= h_1(W) \cdot h_2(W; \rho_d) \\ &= h_1(W) [h_1(W) - (\rho_d) \delta(r)] \\ &= h_1^2(W) - (\rho_d) \delta(r) h_1(W) \end{aligned} \tag{21}$$

The 1<sup>st</sup> term is the effective or resultant PSF for perfect alignment of both objectives of linear apertures while the 2<sup>nd</sup> term  $= (\rho_d) \delta(r) h_1(W)$  is the aberration due to misalignment corresponding to the 2<sup>nd</sup> objective.

Following similar procedure for the quadratic aperture using equations (19, 20), we get the following result for the effective PSF as:

$$\begin{aligned} h_4(W; \rho_d) &= h_3(W) - 2(\rho_d) h_1(W) + \rho_d^2 \delta(r) \\ h_{eff}(\text{quadratic apert.}) &= h_3(W) \cdot h_4(W; \rho_d) \\ &= h_3(W) [h_3(W) - 2(\rho_d) h_1(W) + \rho_d^2 \delta(r)] \\ &= h_3^2(W) - 2(\rho_d) h_1(W) h_3(W) + \rho_d^2 \delta(r) h_3(W) \end{aligned} \tag{22}$$

The 1<sup>st</sup> term in equation (22) represents the effective or resultant PSF for perfect alignment of both objectives of quadratic apertures while the sum of the 2<sup>nd</sup> and 3<sup>rd</sup> terms is the aberration due to misalignment of the 2<sup>nd</sup> objective.

Hence, the misalignment aberration term due to shifted quadratic aperture is given as follows:

$$g(W; \rho_d) = [\rho_d^2 \delta(r) - 2(\rho_d) h_1(W)] h_3(W) \tag{23}$$

It is clear that for perfectly aligned optical system for the objectives of the CSLM, the misaligned term in equation (23) is disappeared since  $\rho_d = 0$  as expected.

Following the analysis made in ref. [18] for circular apertures where the second objective of the CSLM is subjected to tilting and to a lateral shift, we obtain for the misaligned linear and quadratic apertures the following results:

For collimated laser beam, assume that the 2<sup>nd</sup> objective is subjected to only a lateral shift  $\rho_d$ , the radial Bessel integral is written for the linear aperture as follows:

$$h_2(W; \rho_d) = 2\pi \int_{-\rho_{02} + \rho_d}^{\rho_{02} + \rho_d} \rho J_0\left(\frac{2\pi\rho r}{\lambda f}\right) \rho d\rho \tag{24}$$

Using the properties of Bessel function and integration by parts in, we finally get the following result for shifted objective having linear aperture:

$$\begin{aligned}
 h_{2 \text{ linear}} (W; \rho_d) &= 4\pi (\rho_{02} + \rho_d)^3 \left\{ \left[ \frac{J_1(W_H)}{W_H} + \frac{J_0(W_H)}{W_H^2} - 2 \sum_i \frac{J_i(W_H)}{W_H^3} \right] \right. \\
 &\quad \left. - \left( \frac{\varepsilon - 1}{\varepsilon + 1} \right)^3 \left[ \frac{J_1(W_L)}{W_L} + \frac{J_0(W_L)}{W_L^2} - 2 \sum_i \frac{J_i(W_L)}{W_L^3} \right] \right\} \quad (25)
 \end{aligned}$$

For the shifted quadratic aperture, we solve the following radial integral:

$$h_4 (W ; \rho_d) = 2\pi \int_{-\rho_{02} + \rho_d}^{\rho_{02} + \rho_d} \rho^2 J_0 \left( \frac{2\pi\rho r}{\lambda f} \right) \rho d\rho \quad (26)$$

We finally get the PSF for the shifted objective which has quadratic aperture as follows:

$$\begin{aligned}
 h_{4 \text{ quadratic}} (W; \rho_d) &= 4\pi (\rho_{02} + \rho_d)^4 \left\{ \left[ \frac{J_1(W_H)}{W_H} - 2 \frac{J_2(W_H)}{W_H^2} \right] \right. \\
 &\quad \left. - \left( \frac{\varepsilon - 1}{\varepsilon + 1} \right)^4 \left[ \frac{J_1(W_L)}{W_L} - 2 \frac{J_2(W_L)}{W_L^2} \right] \right\} \quad (27)
 \end{aligned}$$

The results of PSF for the shifted objective provided with linear and quadratic apertures in equation 25, 27 are compared with the shifted objective corresponding to circular aperture represented by the following equation (28):

$$h_{2 \text{ circular}} (W; \rho_d) = 4\pi (\rho_{02} + \rho_d)^2 \left\{ \left[ \frac{J_1(W_H)}{W_H} \right] - \left( \frac{\varepsilon - 1}{\varepsilon + 1} \right)^2 \left[ \frac{J_1(W_L)}{W_L} \right] \right\} \quad (28)$$

where  $\varepsilon = \frac{\rho_d}{\rho_{02}} \ll 1$  in all equations (25), (27), and (28).

Where the upper and lower reduced coordinates are written as follows:

$$W_H = \frac{2\pi(\rho_{02} + \rho_d)}{\lambda f} r = \frac{2\pi}{\lambda} N.A. \left( 1 + \frac{\rho_d}{\rho_{02}} \right) r \quad (29)$$

$$W_L = \frac{2\pi(-\rho_{02} + \rho_d)}{\lambda f} r = \frac{2\pi}{\lambda} N.A. \left( \frac{\rho_d}{\rho_{02}} - 1 \right) r \quad (30)$$

The numerical aperture corresponding to the second objective is,  $NA = \frac{\rho_{02}}{f}$  and f is its focal length.

It is known that the CTF for the CSLM is computed from the convolution product corresponding to the apertures of the microscope objectives. It gives maximum value of unity in the center and decreases until reaches zero when the two apertures are completely separated. When the microscope objectives are affected by a displacement in its plane, the maximum value of the CTF is decreased as expected.

An empirical formula for the maximum value of the CTF is given corresponding to one aligned objective with quadratic or linear aperture while the second has the same aperture distribution but displaced by an amount of delta ro. The aperture radius =ro

$$C(\rho) = P_1(\rho) * P_2(\rho) \quad (31)$$

Then,  $C_{max}(\rho = 0) = 1$  ; two aligned objectives each has either linear or quadratic aperture.

In case, of one aligned objective of one aligned linear or quadratic aperture and the 2<sup>nd</sup> objective has misaligned linear or quadratic aperture, the maximum value of the CTF is expressed by the following empirical formula:

$$C_{max}(\delta\rho) = \exp[-\alpha\pi(\delta\rho/\rho_0)] \quad (32)$$

Where  $\alpha$  is a parameter, its value is dependent on the aperture distribution. The maximum value of the CTF becomes unity when the displacement  $\delta\rho = 0$ .

The contrast of the output images in the CSLM is computed using either of these formulae:

$$\text{Contrast} = I_{\max} / I_{\min} \quad (33)$$

Or

$$\text{Contrast} = 1 + [0.5 * (I_{\max} - I_{\min}) / I_{\max}] \quad (34)$$

The accurate method to compute the contrast of an image is based on computing the standard deviation (root mean square) of pixel luminance in an image, divided by the average luminance of the whole image. The formula for computation is as follows:

$$\text{Contrast} = \left( \frac{1}{N \times M} \right) \frac{\text{sqrt} \left\{ \sum_{i=1}^M \sum_{j=1}^N (L(i,j) - \langle L \rangle)^2 \right\}}{\langle L \rangle} \quad (35)$$

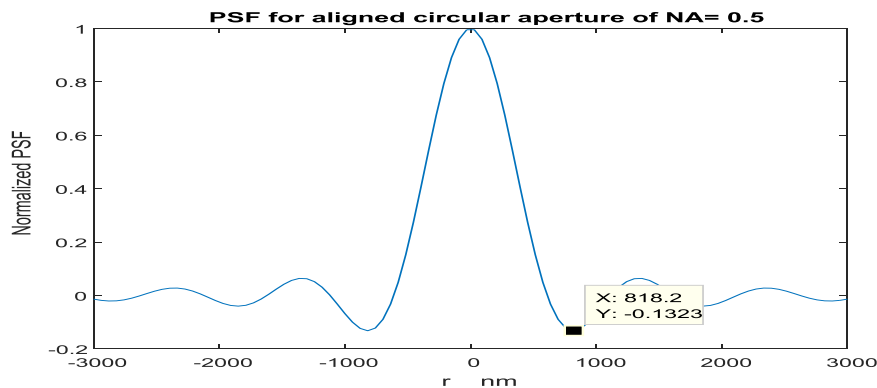
Where the average luminance  $\langle L \rangle$  is calculated as follows:

$$\langle L \rangle = \left( \frac{1}{N \times M} \right) \sum_{i=1}^M \sum_{j=1}^N L(i,j) \quad (36)$$

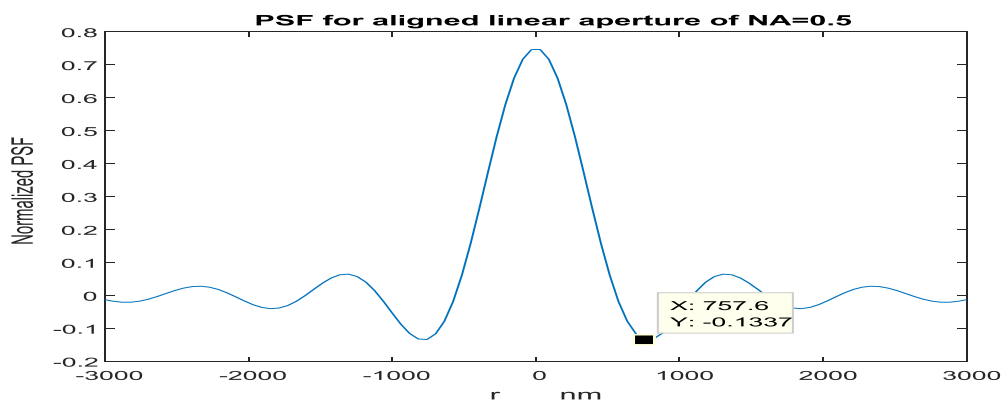
### RESULTS AND DISCUSSION

We have considered the PSF of aligned and misaligned circular apertures. In Fig. (2-a) we considered the PSF of aligned circular aperture for the 1<sup>st</sup> objective. The cut-off spatial frequency is  $r_c / \lambda f = 818.2 \text{ nm} / \lambda f$ , for  $\text{NA} = 0.5$ . In Fig. (2-b) we consider the PSF of linear aperture for the 1<sup>st</sup> objective. The cut-off spatial frequency is  $r_c / \lambda f = 757.6 \text{ nm} / \lambda f$ , for  $\text{NA} = 0.5$ . In Fig. (2-c) we consider the PSF of aligned quadratic aperture for the 1<sup>st</sup> objective. The cut-

off spatial frequency is  $r_c / \lambda f = 697 \text{ nm} / \lambda f$ , for  $\text{NA} = 0.5$ . From the three figures we find that quadratic aperture has narrower main lobe than that of linear aperture. Further, the linear aperture has main lobe narrower than that of uniform circular aperture, as expected. In Fig. (3-a) we consider the PSF of a displaced linear aperture for the 2<sup>nd</sup> objective, where  $\frac{\rho_d}{\rho_{02}} = 0.1$ . The cut-off spatial frequency is  $r_c / \lambda f = 757.6 \text{ nm} / \lambda f$ , for  $\text{NA} = 0.5$ . In Fig. (3-b) we consider the PSF

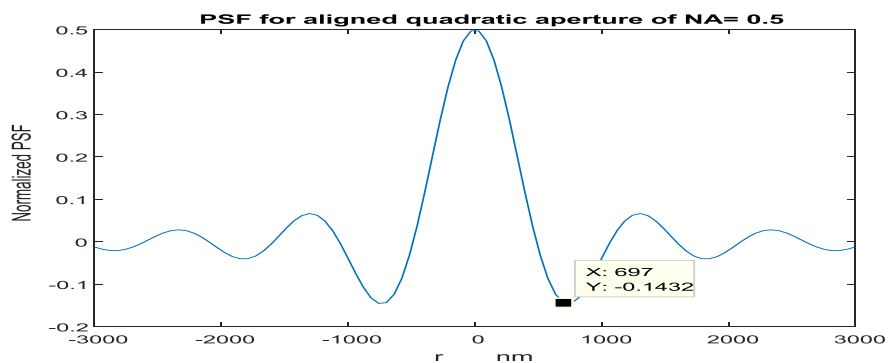


**Figure (2- a):** The PSF using aligned circular aperture for the 1<sup>st</sup> objective. The cut-off spatial frequency is  $r_c / \lambda f = 818.2 \text{ nm} / \lambda f$ , for  $\text{NA} = 0.5$ . Two complete side lobes are shown on the graph for  $r_{\max} = 3000 \text{ nm}$ .



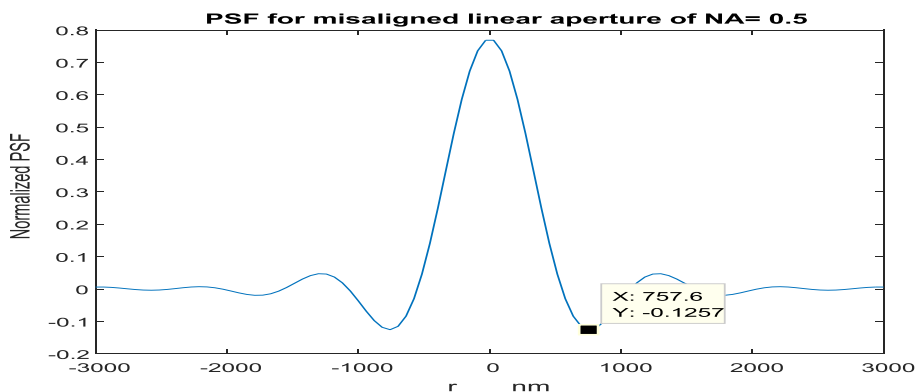
**Figure (2- b):** The PSF using aligned linear aperture for the 1<sup>st</sup> objective. The cut-off spatial frequency is  $r_c / \lambda f = 757.6 \text{ nm} / \lambda f$ , for  $\text{NA} = 0.5$ . Two complete side lobes are shown on the graph for  $r_{\max} = 3000 \text{ nm}$ .



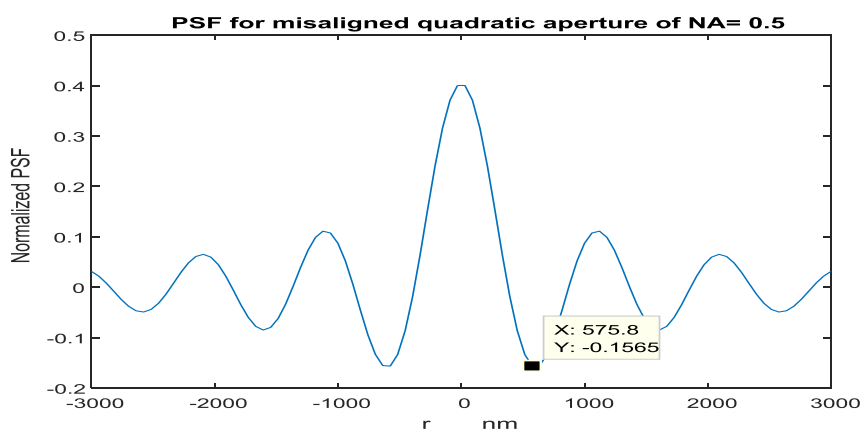


**Figure (2- c):** The PSF using aligned quadratic aperture for the 1<sup>st</sup> objective. The cut- off spatial frequency is  $r_c / \lambda f = 697 \text{ nm} / \lambda f$ , for NA = 0.5.

Two complete side lobes are shown on the graph for  $r_{\text{max}} = 3000 \text{ nm}$ . of a displaced quadratic aperture for the 2<sup>nd</sup> objective, where  $\frac{\rho_d}{\rho_{02}} = 0.1$ . The cut- off spatial frequency is  $r_c / \lambda f = 575.8 \text{ nm} / \lambda f$ , for NA = 0.5. From these two figures we can find that the quadratic aperture has a PSF that is narrower than that of linear aperture, as compared with the similar results for the aligned apertures.



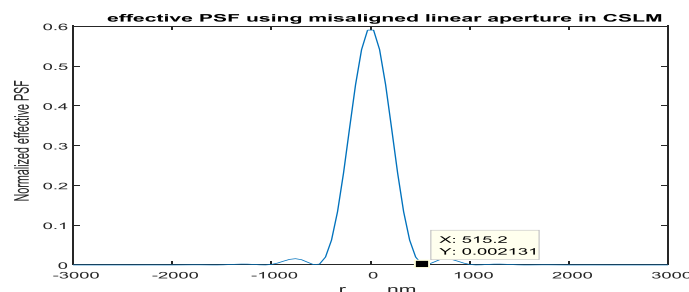
**Figure (3- a):** The PSF using displaced linear aperture for the 2<sup>nd</sup> objective, where  $\frac{\rho_d}{\rho_{02}} = 0.1$ . The cut- off spatial frequency is  $r_c / \lambda f = 757.6 \text{ nm} / \lambda f$ , for NA = 0.5.



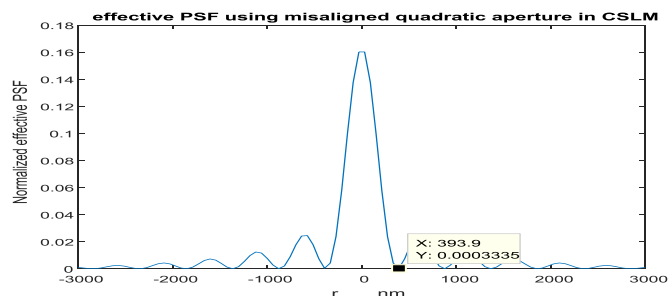
**Figure (3- b):** The PSF using displaced quadratic aperture for the 2<sup>nd</sup> objective, where  $\frac{\rho_d}{\rho_{02}} = 0.1$ . The cut- off spatial frequency is  $r_c / \lambda f = 575.8 \text{ nm} / \lambda f$ , for NA = 0.5.

In Fig. (4-a) we consider the effective PSF of only using displaced linear aperture for the 2<sup>nd</sup> objective, where  $\frac{\rho_d}{\rho_{02}} = 0.1$ . The cut- off spatial frequency is  $r_c / \lambda f = 515.2 \text{ nm} / \lambda f$ , for NA = 0.5. In Fig. (4-b) we consider The effective PSF using only displaced quadratic

aperture for the 2<sup>nd</sup> objective, where  $\frac{\rho_d}{\rho_{02}} = 0.1$ . The cut- off spatial frequency is  $r_c / \lambda f = 393.9 \text{ nm} / \lambda f$ , for NA = 0.5. Again for the misaligned case we have effective PSF narrower for the quadratic case than that for the linear aperture.



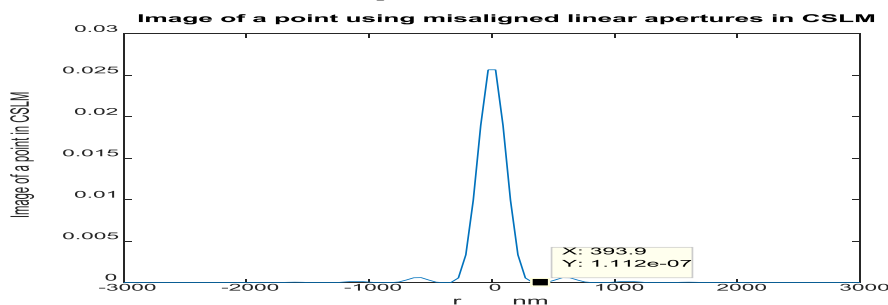
**Figure (4- a):** The effective or resultant PSF using displaced linear aperture for the 2<sup>nd</sup> objective, where  $\frac{\rho_d}{\rho_{02}} = 0.1$ . The cut- off spatial frequency is  $r_c / \lambda f = 515.2 \text{ nm}/\lambda f$ , for  $NA = 0.5$ .



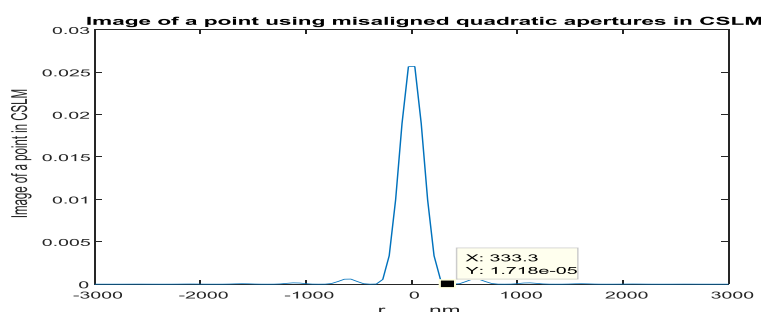
**Figure (4- b):** The effective or resultant PSF using displaced quadratic aperture for the 2<sup>nd</sup> objective, where  $\frac{\rho_d}{\rho_{02}} = 0.1$ . The cut- off spatial frequency is  $r_c / \lambda f = 393.9 \text{ nm}/\lambda f$ , for  $NA = 0.5$ .

In addition, we have only one side lobe in the effective PSF using displaced linear aperture for the 2<sup>nd</sup> objective as shown in the figure (4- a), while many lobes are shown in case of displaced quadratic aperture as shown in the figure (4- b). In Fig. (5-a) we consider the image of a point using two misaligned linear apertures in the CSLM where  $NA = 0.5$ . The cut- off spatial

frequency is  $r_c / \lambda f = 393.9 \text{ nm}/\lambda f$ . In Fig. (5- b) we consider the image of a point using two misaligned quadratic apertures in the CSLM where  $NA = 0.5$ . The cut- off spatial frequency is  $r_c / \lambda f = 333.3 \text{ nm}/\lambda f$ . In both figures we have only one side lobe and the other is highly suppressed. Again, in the quadratic case we get a curve that narrower than that of the linear one.



**Figure (5- a):** The plot represents the image of a point using two misaligned linear apertures in the CSLM where  $NA = 0.5$ . The cut- off spatial frequency is  $r_c / \lambda f = 393.9 \text{ nm}/\lambda f$ .

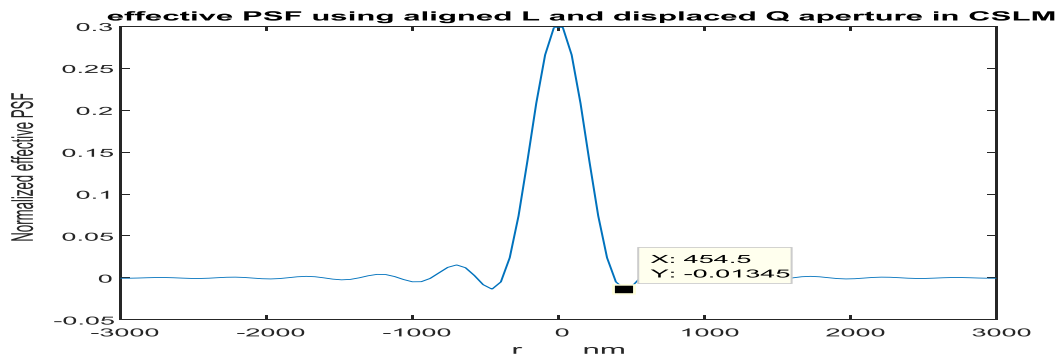


**Figure (5- b):** The plot represents the image of a point using two misaligned quadratic apertures in the CSLM where  $NA = 0.5$ . The cut- off spatial frequency is  $r_c / \lambda f = 333.3 \text{ nm}/\lambda f$ . One side loop is shown while the others are truncated.



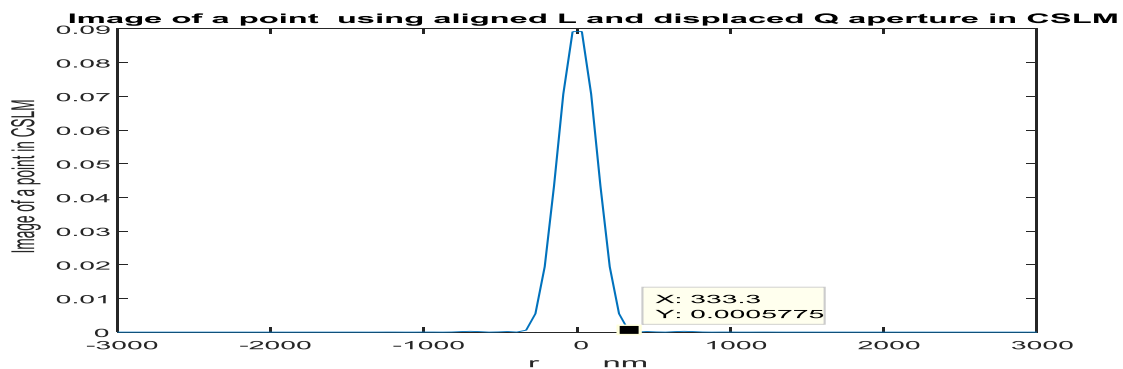
In Fig. (6-a) we consider the effective PSF of using aligned linear aperture for the 1<sup>st</sup> objective, while the 2<sup>nd</sup> objective with quadratic aperture is displaced by  $\rho_d$ , where  $\frac{\rho_d}{\rho_{02}} = 0.1$ . The cut-off spatial frequency is  $r_c / \lambda f = 454.5 \text{ nm}/\lambda f$ , for NA = 0.5 for both apertures. From the figure we find highly attenuated side lobes. In Fig. (6-b)

we consider the image of a point using aligned linear aperture for the 1<sup>st</sup> objective, while the 2<sup>nd</sup> objective with quadratic aperture is displaced by  $\rho_d$ , where  $\frac{\rho_d}{\rho_{02}} = 0.1$ . The cut-off spatial frequency is  $r_c / \lambda f = 333.3 \text{ nm}/\lambda f$ , for NA = 0.5 for both apertures. It is clear from the figure that side lobes are totally suppressed.



**Figure (6- a):** The effective or resultant PSF using aligned linear aperture for the 1<sup>st</sup> objective, while the 2<sup>nd</sup> objective with quadratic aperture is displaced by  $\rho_d$ , where  $\frac{\rho_d}{\rho_{02}} = 0.1$ .

The cut-off spatial frequency is  $r_c / \lambda f = 454.5 \text{ nm}/\lambda f$ , for NA = 0.5 for both apertures. It is shown that, the side loops are attenuated.



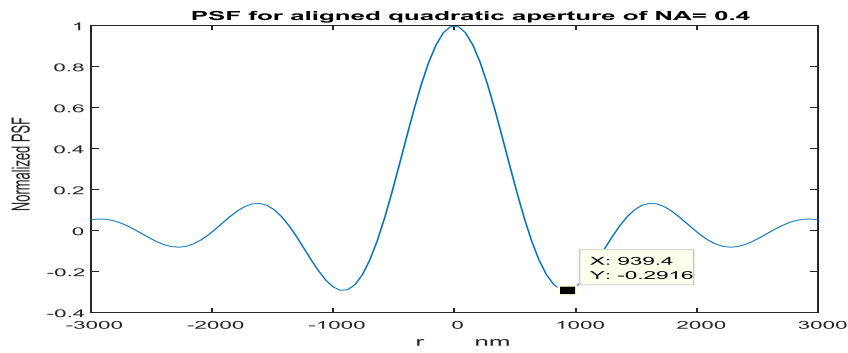
**Figure (6- b):** The image of a point using aligned linear aperture for the 1<sup>st</sup> objective, while the 2<sup>nd</sup> objective with quadratic aperture is displaced by  $\rho_d$ , where  $\frac{\rho_d}{\rho_{02}} = 0.1$ .

The cut-off spatial frequency is  $r_c / \lambda f = 333.3 \text{ nm}/\lambda f$ , for NA = 0.5 for both apertures. It is shown that, the side loops are disappeared or truncated.

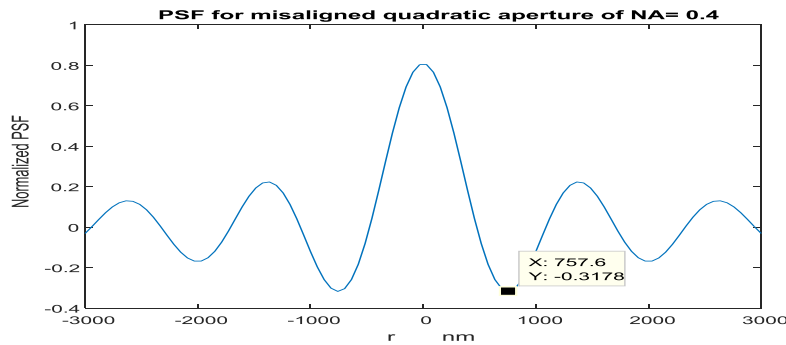
quadratic aperture with NA=0.4 we have the 1<sup>st</sup> secondary peak located at 1606 nm. In Fig. (7-d) we have the PSF of misaligned quadratic aperture with NA=0.4. From the figure we can see that the 1<sup>st</sup> secondary peak located at 1364 nm. 10% lateral shift w.r.t the maximum radius of the quadratic aperture is assumed.

In Fig. (7-a) we consider the PSF of aligned quadratic aperture for the 1<sup>st</sup> objective. The cut-off spatial frequency is  $r_c / \lambda f = 939.4 \text{ nm}/\lambda f$ . NA = 0.4. In Fig. (7-b) we consider the PSF of misaligned quadratic aperture for the 2<sup>nd</sup> objective, subjected to a lateral shift where  $\frac{\rho_d}{\rho_{02}} = 0.1$  and NA = 0.4. The cut-off spatial frequency is  $r_c / \lambda f = 757.6 \text{ nm}/\lambda f$ . We can see from these two figures that the PSF in the misaligned case is narrower than that of the aligned. In Fig. (7-c) we have the PSF of aligned

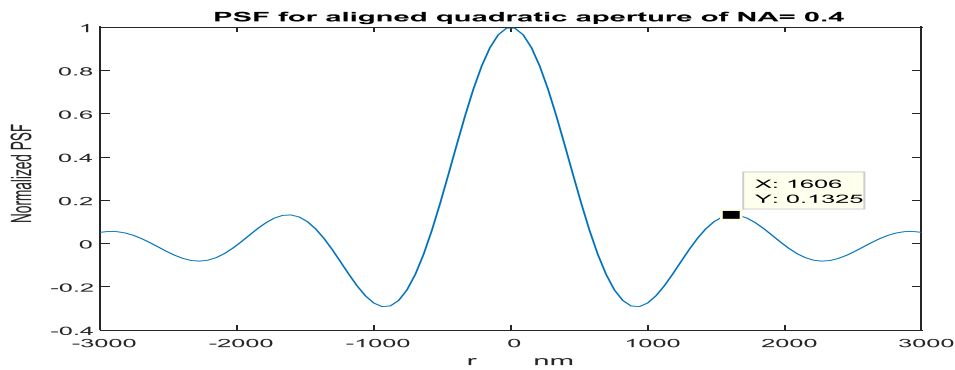
The central peak has nearly 0.8 as compared with unity for the aligned quadratic aperture. In Fig. (7-e) we consider the PSF aligned and misaligned quadratic aperture. In this figure we can find that the 1<sup>st</sup> secondary peaks in the PSF of the 1<sup>st</sup> aligned objective and the 2<sup>nd</sup> displaced objective located at 1727, 1364 nm respectively. The displacement corresponding to the 2<sup>nd</sup> objective has 0.1 the aperture radius.



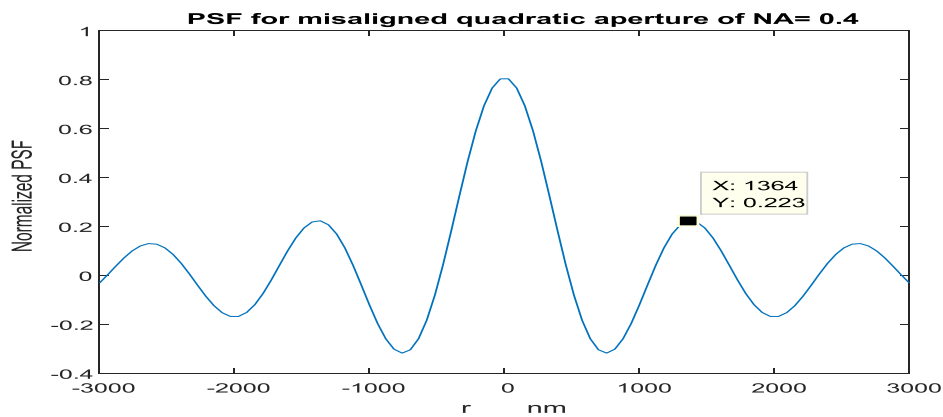
**Figure (7- a):** The PSF using aligned quadratic aperture for the 1<sup>st</sup> objective. The cut- off spatial frequency is  $r_c / \lambda f = 939.4 \text{ nm}/\lambda f$ .  $NA = 0.4$ . One and nearly half side lobes are shown on the graph for  $r_{max} = 3000 \text{ nm}$ .



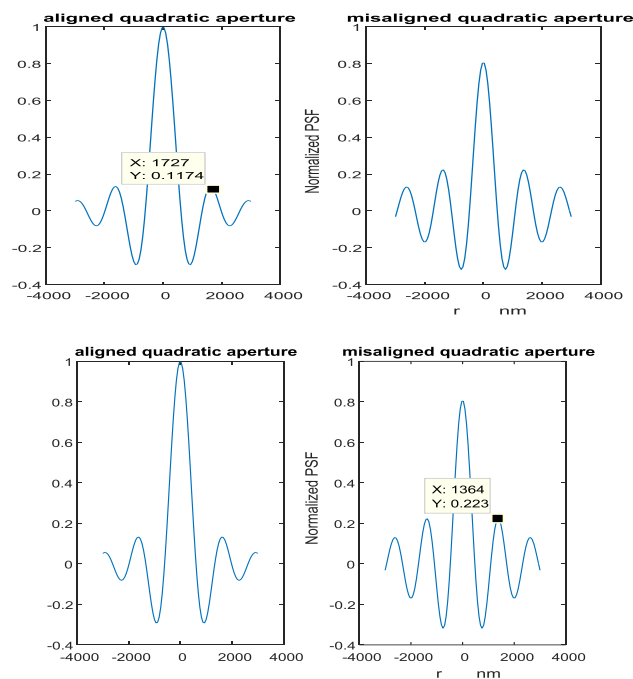
**Figure (7- b):** The PSF using misaligned quadratic aperture for the 2<sup>nd</sup> objective, subjected to a lateral shift where  $\frac{\rho_d}{\rho_{02}} = 0.1$  and  $NA = 0.4$ . The cut- off spatial frequency is  $r_c / \lambda f = 757.6 \text{ nm}/\lambda f$ . Two complete side lobes are shown on the graph for  $r_{max} = 3000 \text{ nm}$ .



**Figure (7- c):** The 1<sup>st</sup> secondary peak located at 1606 nm.



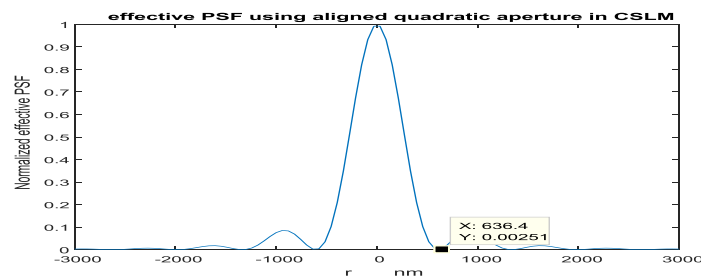
**Figure (7- d):** The 1<sup>st</sup> secondary peak located at 1364 nm. 10% lateral shift w.r.t the maximum radius of the quadratic aperture is assumed. The central peak has nearly 0.8 as compared with unity for the aligned quadratic aperture.



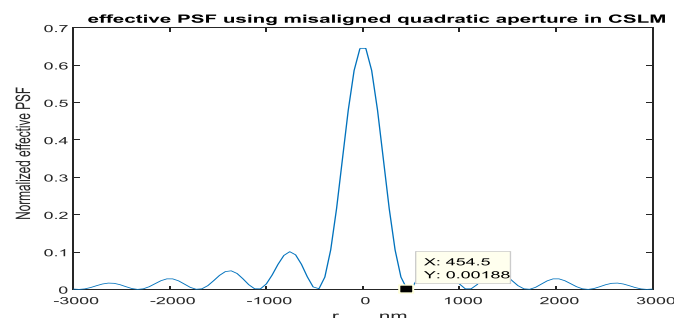
**Figure (7- e):** The 1<sup>st</sup> secondary peaks in the PSF of the 1<sup>st</sup> aligned objective and the 2<sup>nd</sup> displaced objective located at 1727, 1364 nm respectively. The displacement corresponding to the 2<sup>nd</sup> objective has 0.1 the aperture radius.

In Fig. (8-a) we consider the effective PSF of two aligned quadratic apertures for the objectives of the CSLM. The cut- off spatial frequency is reduced to  $r_c / \lambda f = 636.4 \text{ nm}/\lambda f$ . In Fig. (8-b) we consider the effective PSF of two misaligned quadratic apertures for the objectives of the CSLM. Both of the microscope objectives are subjected to a lateral shift where

$\frac{\rho_d}{\rho_{02}} = 0.1$ . The cut- off spatial frequency is  $r_c / \lambda f = 454.5 \text{ nm}/\lambda f$  with  $\text{NA} = 0.4$ . From these two figure we can find that: first, the central lobe in the misaligned case is narrower than that of the aligned case. Second, the side lobes in the aligned case die out faster than that of the misaligned case.



**Figure (8- a):** The RPSF using two aligned quadratic apertures for the objectives of the CSLM. The cut- off spatial frequency is reduced to  $r_c / \lambda f = 636.4 \text{ nm}/\lambda f$ .

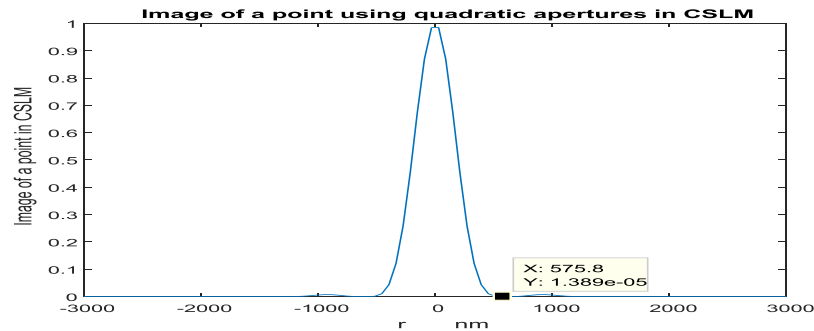


**Figure (8- b):** The effective or RPSF using two misaligned quadratic apertures for the objectives of the CSLM. Both of the microscope objectives are subjected to a lateral shift where  $\frac{\rho_d}{\rho_{02}} = 0.1$ . The cut- off spatial frequency is  $r_c / \lambda f = 454.5 \text{ nm}/\lambda f$  becomes maximum , at  $\text{NA} = 0.4$ .

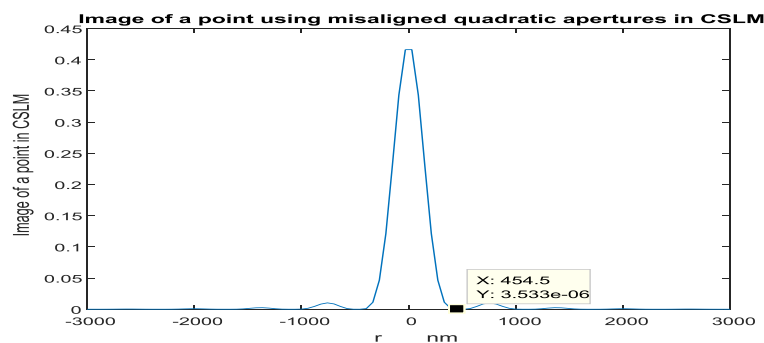
## A Study on Misaligned Modulated Apertures in Confocal Scanning Laser Microscope (CSLM)

In Fig. (9-a) we consider the image of a point using two aligned quadratic apertures in the CSLM where  $NA = 0.4$ . The cut-off spatial frequency is  $r_c / \lambda f = 575.8 \text{ nm}/\lambda f$ . In Fig. (9-b) we consider the image of a point using two misaligned quadratic apertures in the CSLM where  $NA = 0.4$ . The cut-off spatial frequency

is  $r_c / \lambda f = 454.5 \text{ nm}/\lambda f$ . The lateral shift is  $r_{0d} = 0.1 \rho_0$  for both of the objectives. From these two figures we find that the image for misaligned case has a narrower central lobe than that of the aligned case. On the other side, side lobes have a smaller level in the aligned case than that of the misaligned case.



**Figure (9- a):** The plot represents the image of a point using two aligned quadratic apertures in the CSLM where  $NA = 0.4$ . The cut-off spatial frequency is  $r_c / \lambda f = 575.8 \text{ nm}/\lambda f$ .



**Figure (9- b):** The plot represents the image of a point using two misaligned quadratic apertures in the CSLM where  $NA = 0.4$ . The cut-off spatial frequency is  $r_c / \lambda f = 454.5 \text{ nm}$ . The lateral shift is  $r_{0d} = 0.1 \rho_0$  for both of the objectives.

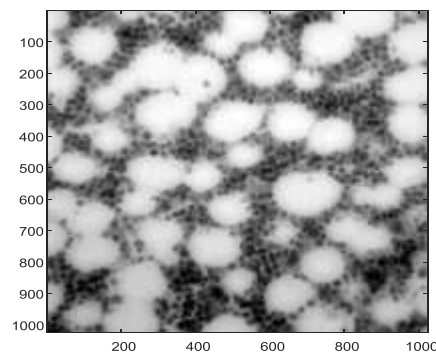
**Table1.** The normalized maximum value of the CTF ( $C_{max}$ ), for the modulated quadratic apertures in the CSLM. The 1<sup>st</sup> objective is aligned while the 2<sup>nd</sup> objective is displaced by an amount =  $\delta r_0$ .

C max	Displacement ( $\delta r$ ) in pixels
1.0	0
1.0	1
0.9925	2
0.9852	3
0.9778	4
0.9725	5
0.9343	10
0.899	15
0.8662	20
0.8338	25
0.8024	30
0.7721	35
0.7428	40
0.7127	45
0.6872	50
0.6608	55
0.6355	60
0.6109	65
0.5876	70
0.5649	75

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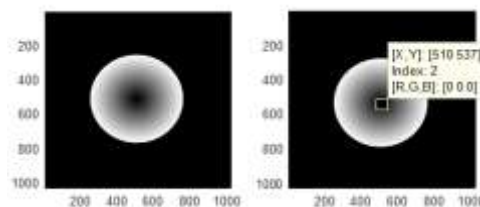
In Fig. (10-a) we consider Bone marrow image of dimensions  $1024 \times 1024$  pixels used in the processing. In Fig.(10-b) we consider linear apertures in image of  $1024 \times 1024$  pixels and radius = 256 pixels. One is centered at (512, 512) pixels, while the other is shifted vertically by a displacement of = 25 pixels. In Fig. (10-c) we consider the Coherent Transfer Function (CTF) computed from direct convolution and FFT technique for the CSLM, where  $CTF = P_1 \otimes P_2$  and  $P_1$  and  $P_2$  for linearly distributed apertures. For FFT calculation peak occurs at 513 pixels. In Fig. (10-d) we consider the CTF computed from direct convolution and FFT technique for the CSLM, where  $P_1$  has aligned linear distribution while  $P_2$  has misaligned linear distribution with displacement = 25 pixels. For FFT calculation peak occurs at 513 pixels. In Fig. (10-e) we consider the output image from the bone marrow image using the CSLM provided with aligned linear apertures for both

of the microscope objectives. In the Fig. (10-f) we consider the output image from the bone marrow image using the CSLM provided with one aligned linear aperture and the 2<sup>nd</sup> has the same linear distribution like the 1<sup>st</sup> but it is displaced vertically by an amount 25 pixels. In Fig. (10-g) we consider the output image from the bone marrow image using the CSLM provided with two misaligned linear apertures for the microscope objectives. The displacement 25 pixels along y- coordinate is assumed in all plots. In Fig. (11-a) we consider two quadratic apertures and radius = 256 pixels in images of  $1024 \times 1024$  pixels. One aperture is centered at (512, 512) pixels, while that the other is shifted vertically by a displacement of = 25 pixels. In Fig. (11-b) we consider the CTF computed from direct convolution and FFT technique for the CSLM, where both of  $P_1$  and  $P_2$  have quadratic distributed apertures. For

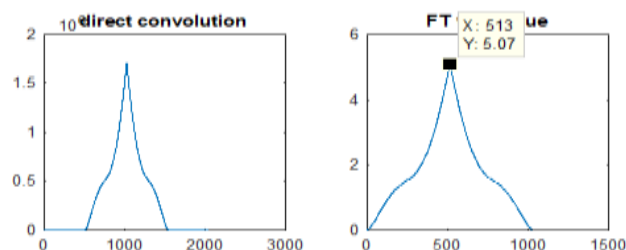


FT calculation peak occurs at 513.

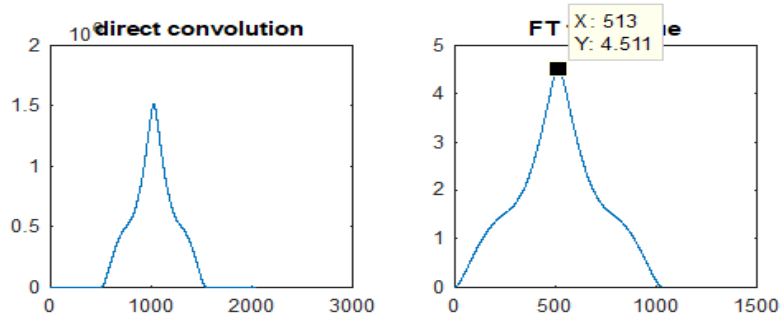
**Figure (10- a):** Bone marrow image of dimensions  $1024 \times 1024$  pixels used in the processing.



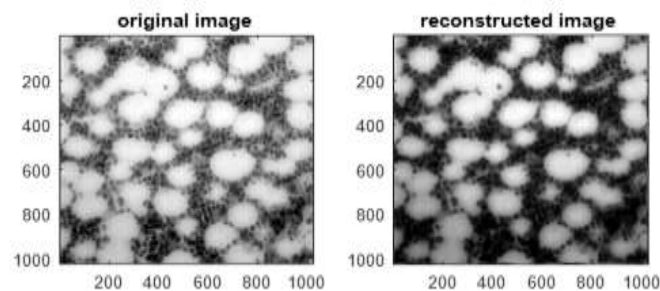
**Figure (10- b):** Two images of linear apertures of dimensions  $1024 \times 1024$  pixels, and radius = 256 pixels. The image in the left, is centered at (512, 512) pixels, while that shown in the right is shifted vertically by a displacement of  $d = 537 - 512 = 25$  pixels.



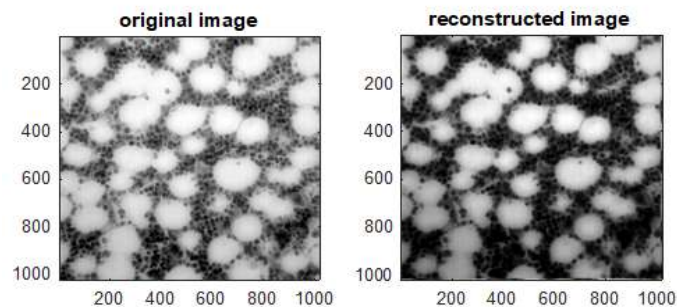
**Figure (10- c):** The Coherent Transfer Function (CTF) computed from direct convolution and FFT technique for the CSLM, where  $CTF = P_1 \otimes P_2$  and  $P_1$  and  $P_2$  have linearly distributed apertures.



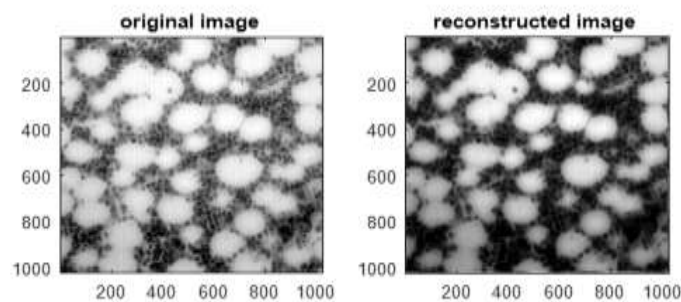
**Figure (10- d):** The Coherent Transfer Function (CTF) computed from direct convolution and FFT technique for the CSLM, where  $CTF = P_1 \otimes P_2$  and  $P_1$  has aligned linear distribution while  $P_2$  has misaligned linear distribution with displacement = 25 pixels.



**Figure (10- e):** The reconstructed image from the bone marrow image using the CSLM provided with aligned linear apertures for both of the microscope objectives.



**Figure (10- f):** The reconstructed image from the bone marrow image using the CSLM provided with one aligned linear aperture and the 2<sup>nd</sup> has the same linear distribution like the 1<sup>st</sup> but it is displaced vertically by an amount 25 pixels.



**Figure (10- g):** The reconstructed image from the bone marrow image using the CSLM provided with two misaligned linear apertures for the microscope objectives. The displacement is 25 pixels along y- coordinate as shown in the aperture in figure (10- b).

In Fig. (11-c) we consider the CTF computed from direct convolution and FFT technique for the CSLM, where  $P_1$  has aligned quadratic distribution while  $P_2$  has misaligned quadratic

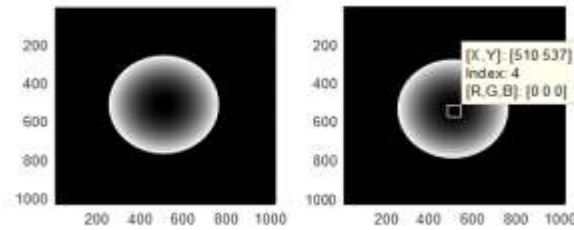
distribution with displacement = 25 pixels. For FFT calculation peak occurs at 514. In Fig. (11- d) we consider the reconstructed image from the bone marrow image using the CSLM provided



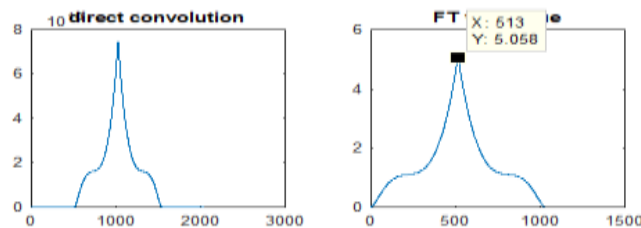
## A Study on Misaligned Modulated Apertures in Confocal Scanning Laser Microscope (CSLM)

with aligned quadratic apertures for the microscope objectives. In Fig. (11-e) we consider the reconstructed image from the bone marrow image using the CSLM provided with

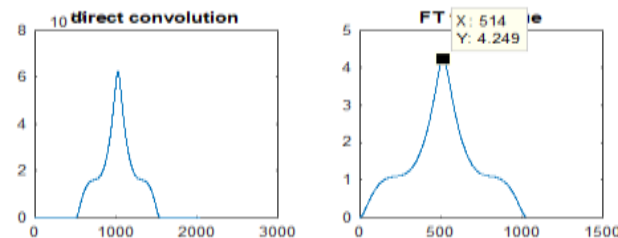
one aligned quadratic aperture and the 2<sup>nd</sup> has the same quadratic distribution like the 1<sup>st</sup> but it is displaced vertically by an amount = 25 pixels.



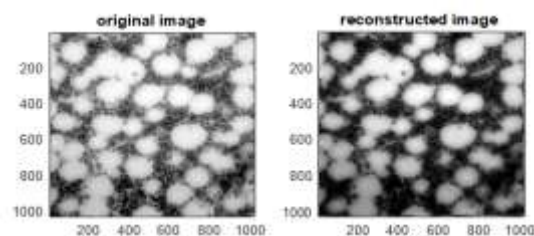
**Figure (11- a):** Two images of quadratic apertures of dimensions  $1024 \times 1024$  pixels, and radius = 256 pixels. The image in the left, is centered at (512, 512) pixels, while that shown in the right is shifted vertically by a displacement of  $d = 537 - 512 = 25$  pixels.



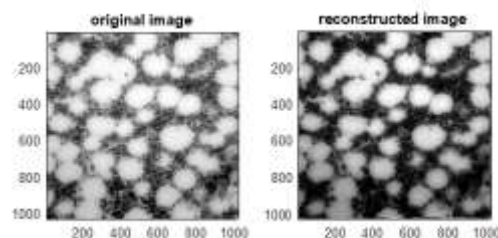
**Figure (11- b):** The Coherent Transfer Function (CTF) computed from direct convolution and FFT technique for the CSLM, where  $CTF = P_1 \otimes P_2$  and both of  $P_1$  and  $P_2$  have quadratic distributed apertures.



**Figure (11- c):** The Coherent Transfer Function (CTF) computed from direct convolution and FFT technique for the CSLM, where  $CTF = P_1 \otimes P_2$  and  $P_1$  has aligned quadratic distribution while  $P_2$  has misaligned quadratic distribution with displacement,  $\delta = 25$  pixels.



**Figure (11- d):** The reconstructed image from the bone marrow image using the CSLM provided with aligned quadratic apertures for the microscope objectives.

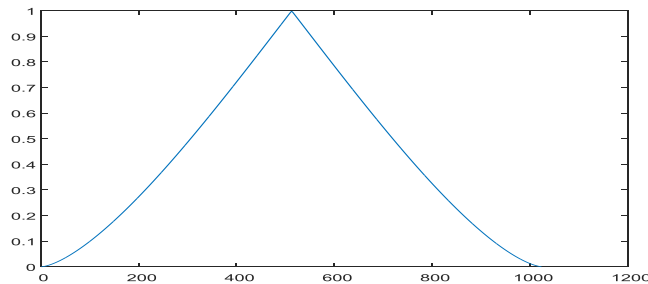


**Figure (11- e):** The reconstructed image from the bone marrow image using the CSLM provided with one aligned quadratic aperture and the 2<sup>nd</sup> has the same quadratic distribution like the 1<sup>st</sup> but it is displaced vertically by an amount  $d = 25$  pixels.

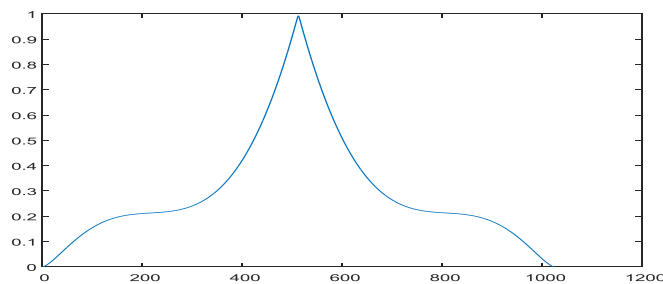
## A Study on Misaligned Modulated Apertures in Confocal Scanning Laser Microscope (CSLM)

we consider normalized plot of the CTF using FFT technique in all the plots shown in the figures (12 a- d). For both of  $P_1$  and  $P_2$  have uniform circular apertures, the maximum value of CTF  $C_{max} = 1.0$ , as in the figure (12- a). In Fig. (12-b), For both of  $P_1$  and  $P_2$  have quadratic distributed apertures,  $C_{max} = 1.0$ . In Fig. (12-c), where both of  $P_1$  and  $P_2$  have quadratic

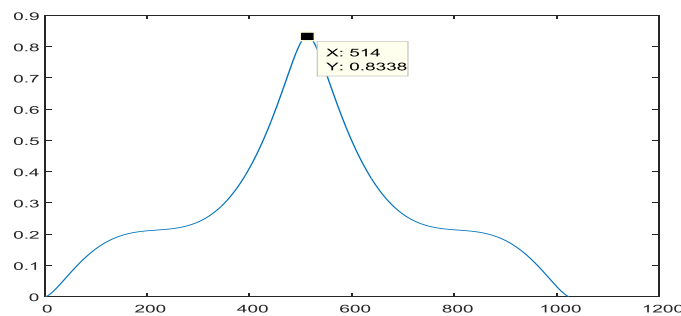
distributed apertures, While the 2<sup>nd</sup> objective is displaced by  $ro = 25$  pixels,  $C_{max} = 0.8338$ . Peak occurs at 514 pixels. In Fig. (12-d), where both of  $P_1$  and  $P_2$  have quadratic distributed apertures, While the 2<sup>nd</sup> objective is displaced by  $ro = 50$  pixels,  $C_{max} = 0.6872$ . The peak occurs at 513 pixels.



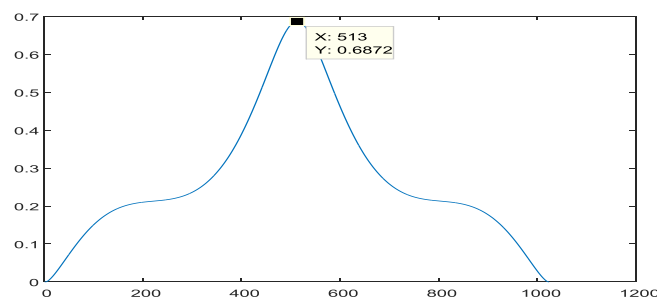
**Figure (12- a):** Normalized plot of the CTF using FFT technique, where  $CTF = P_1 \otimes P_2$  and both of  $P_1$  and  $P_2$  have uniform circular apertures.



**Figure (12- b):** Normalized plot of the CTF using FFT technique, where  $CTF = P_1 \otimes P_2$  and both of  $P_1$  and  $P_2$  have quadratic distributed apertures.  $C_{max} = 1.0$ .



**Figure (12- c):** Normalized plot of the CTF using FFT technique, where  $CTF = P_1 \otimes P_2$  and both of  $P_1$  and  $P_2$  have quadratic distributed apertures. While the 2<sup>nd</sup> objective is displaced by  $ro = 25$  pixels.  $C_{max} = 0.8338$ .

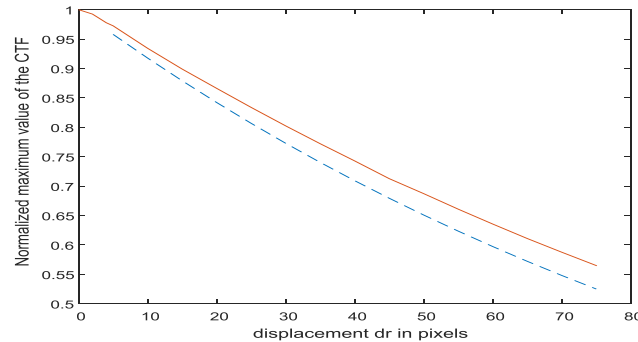


**Figure (12- d):** Normalized plot of the CTF using FFT technique, where  $CTF = P_1 \otimes P_2$  and both of  $P_1$  and  $P_2$  have quadratic distributed apertures. While the 2<sup>nd</sup> objective is displaced by  $ro = 50$  pixels.  $C_{max} = 0.6872$ .

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In Fig. 13 we consider the normalized plot of the maximum value of the CTF as a function of the displacement ( $\delta r_0$ ) in pixels occurred in the 2<sup>nd</sup> objective where the 1<sup>st</sup> objective is assumed aligned. The apertures have quadratic distributions each of radius = 256 pixels. The continuous curve is the maximum CTF

computed from the FFT techniques while the discontinuous curve is computed from the empirical formula where is set equal to  $\alpha = 0.7$ . It is shown that the computed values from FFT and that computed from empirical formula are in good agreement for small displacement.



**Figure (13):** The Normalized plot of the maximum value of the CTF as a function of the displacement ( $\delta r_0$ ) in pixels occurred in the 2<sup>nd</sup> objective where the 1<sup>st</sup> objective is aligned.

The apertures have quadratic distributions each of radius = 256 pixels. The continuous curve is the maximum CTF computed from the FFT

techniques while the discontinuous curve is computed from the empirical formula where  $\alpha = 0.7$ .

**Table 2.** The contrast computed by two methods for the output images versus displacement given to the 2<sup>nd</sup> objective lens considering modulated quadratic apertures in the CSLM. While the 1<sup>st</sup> objective is assumed aligned.

Contrast = $I_{\max} / I_{\min}$	Contrast = $1 + 0.5 * (I_{\max} - I_{\min}) / I_{\max}$	Displacement ( $\delta r_0$ ) in pixels
0.9610	0.9797	0
0.9416	0.9690	2
0.9310	0.9630	3
0.9204	0.9568	4
0.9089	0.9499	5
0.8442	0.9077	10
0.7815	0.8602	15
0.7248	0.8102	20
0.6719	0.7558	25
0.6223	0.6965	30
0.5762	0.6323	35
0.5334	0.5626	40
0.4937	0.4872	45
0.4568	0.4054	50
0.4226	0.3167	55
0.3909	0.2208	60

**Table.** The mean value  $\langle I \rangle$ , the standard deviation  $\sigma$ , and the contrast of the reconstructed images versus displacement given to the 2<sup>nd</sup> objective lens considering modulated quadratic apertures in the CSLM. While the 1<sup>st</sup> objective is assumed aligned.

$\langle I \rangle$	$\sigma = \text{STD}$	Image contrast = $\sigma / \langle I \rangle$	Displacement ( $\delta r_0$ ) in pixels
0.4312	0.2703	0.6267	0
0.4027	0.2570	0.6383	5
0.3746	0.2406	0.6423	10
0.3477	0.2239	0.6438	15
0.3225	0.2079	0.6445	20
0.2990	0.1928	0.6450	25
0.2770	0.1787	0.6453	30
0.2565	0.1656	0.6455	35
0.2374	0.1533	0.6457	40

0.2197	0.1419	0.6458	45
0.2033	0.1313	0.6459	50
0.1880	0.1215	0.6460	55
0.1739	0.1123	0.6461	60

Contrast of the original input image = 0.3908 computed from equations (34, 35).

Mean value = 157.74 /256 = 0.6162

Standard deviation = 61.64 /256 = 0.2408

The results of the image contrast, computed from equation (33) for the reconstructed images in the CSLM, versus objective displacement is shown in the table (2). Where the two microscope objectives are provided with quadratic apertures with the 1<sup>st</sup> objective aligned while the 2<sup>nd</sup> is displaced by an amount .It is shown that the contrast computed from  $I_{max} / I_{min}$  is decreased with aperture displacement as expected. The contrast of the output images is changed from nearly 96 % for two aligned apertures of the microscope objectives to about 39% for displacement = 60 pixels. In addition, the contrast is sensitive to small displacement it decreases from 96% to 90% for nearly 5 pixels.

The accurate formula used to obtain image contrast is computed from equation (34). The results of the mean value  $\langle I \rangle$ , the standard deviation  $\sigma$ , and the contrast of the output images versus displacement given to the 2<sup>nd</sup> objective lens considering modulated quadratic apertures in the CSLM. While the 1<sup>st</sup> objective is assumed aligned are shown in the table (3). It is shown that the contrast of the output images is much improved as compared with the contrast of the input bone marrow image. While it remains nearly constant at about 0.64 for different displacements changed up to nearly 10% with respect to the aperture radius.

### CONCLUSION

We considered aligned and misaligned quadratic apertures. For the case of one misaligned aperture, we have narrower PSF than that for the case of aligned one. Cut-off spatial frequency and position of first peak comes nearer to the main lobe than that of the aligned case. Then we considered the effective PSF for two aligned apertures and two misaligned apertures. Again, in misaligned case the spatial cut-off frequency is lower than that of the aligned case. Moreover, side lobes die faster in the aligned case than that of the misaligned case. Moreover, we considered linear apertures and we found that the PSF has central lobe in the quadratic case narrower than that for the linear. The empirical formula for the maximum CTF outlined in the theoretical analysis is compared with the

corresponding CTF computed from the FFT technique as shown in the plot. Consequently, the degree of misalignment is related to the displacement of the 2<sup>nd</sup> objective for the quadratic aperture. The method is sensitive to displacement of 2 pixels. It is shown that the image contrast is greatly affected by the objective displacement since it changes from 96% to nearly 39% for 10% misalignment. Consequently, the optical confocal system of the microscope is checked for alignment by measuring the image contrast corresponding to the output images computed from  $I_{max} / I_{min}$ .

While the computation of the image contrast from the accurate method of STD showed nearly constant values. While the root mean square values are decreased with the displacement. In addition, the mean values are also decreased with the displacement given to either the aperture or the microscope objective. Hence, this method to check alignment of the optical system of the CSLM is evident by measuring either the mean or the root mean square values separately.

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